



"Synthetic Data in Infrared Thermography for NonDestructive Evaluation"

by
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in collaboration with
François Galmiche and Xavier Maldague

CAP CONGRESS
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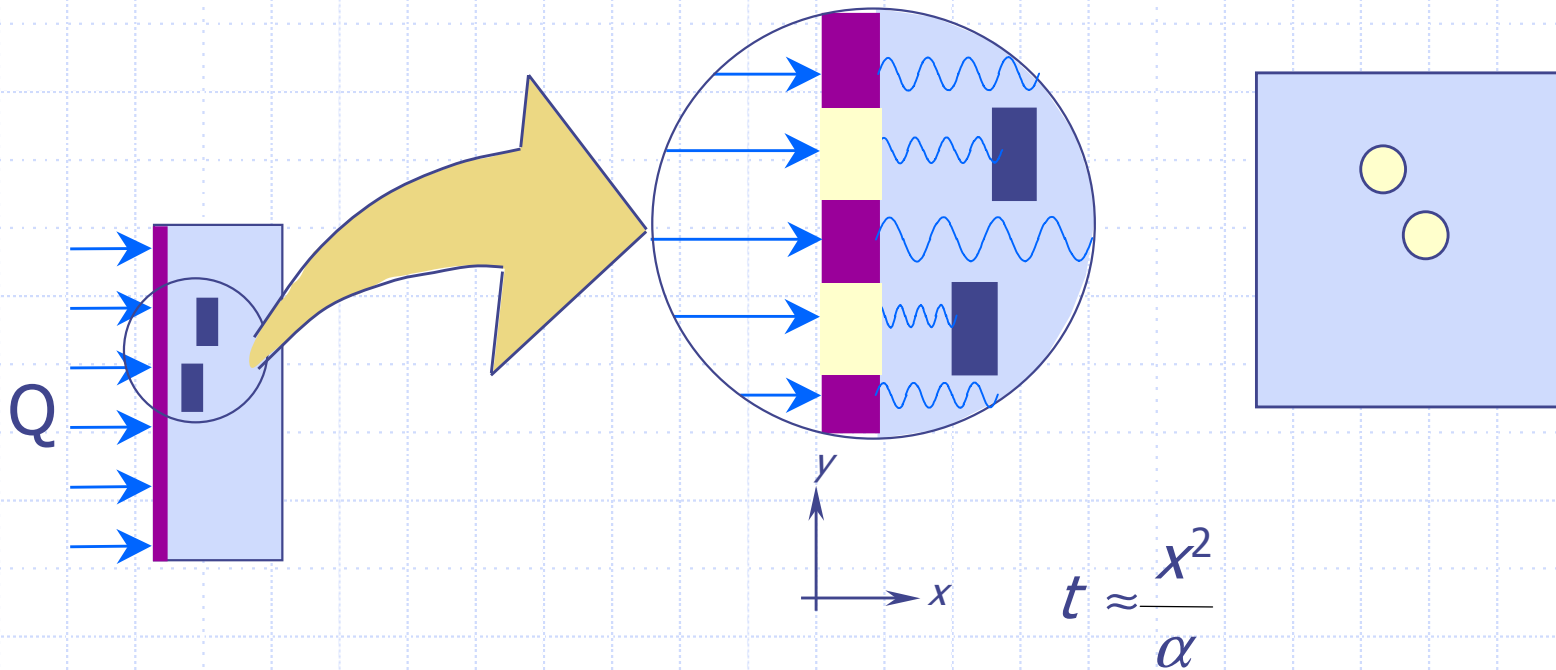
Outline

- ◆ Introduction: IRT for NDE
- ◆ Synthetic Data
- ◆ Experimental Procedures
- ◆ Conclusions & Perspectives



Introduction

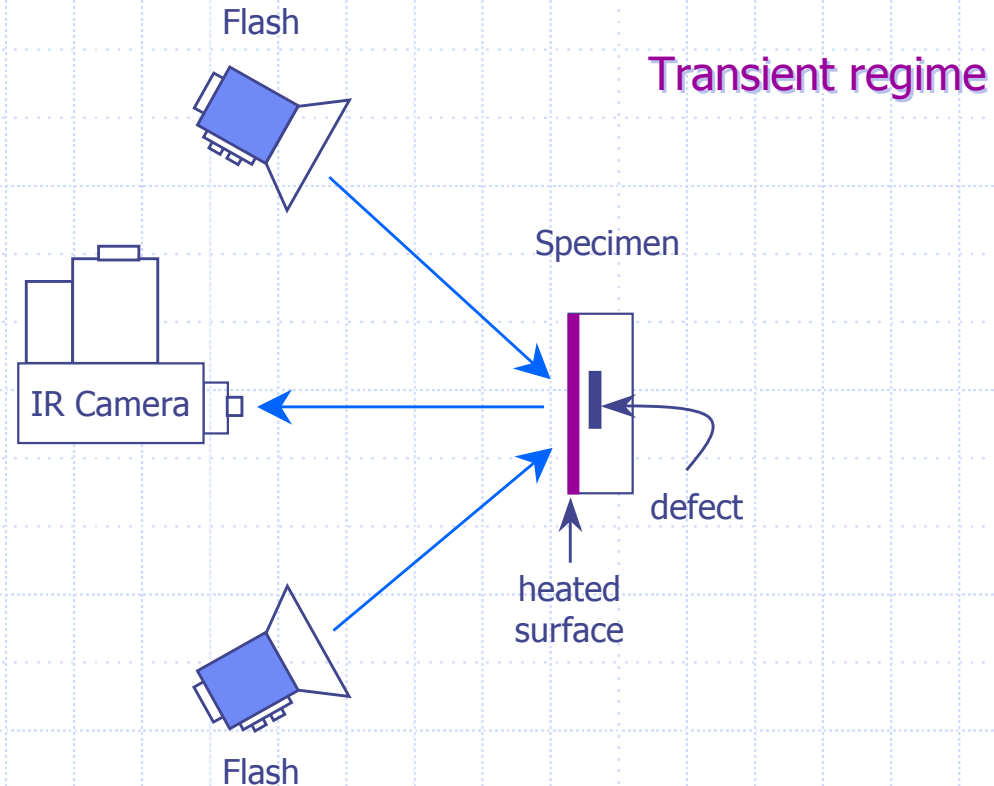
◆ Active Thermography for NDE





Introduction

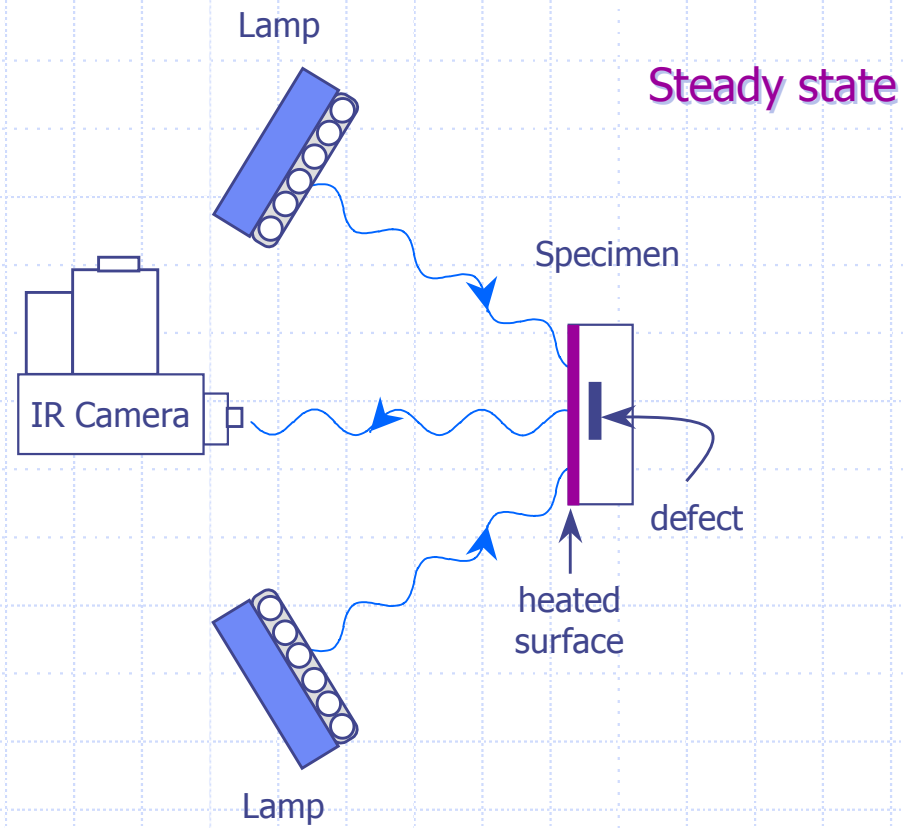
◆ Pulse Thermography, PT





Introduction

◆ Lock-in Thermography, LT



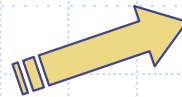


Introduction

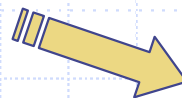
◆ Pulsed Phase Thermography, PPT

- Experimental setup as in PT;
- Fourier Transform \Leftrightarrow frequency domain
- PPT several f (only one f at a time for LT);

$$F_n = \sum T(k) e^{2\pi i k n / N} = \text{Re}_n + i \text{Im}_n$$



$$A = \sqrt{\text{Re}_n^2 + \text{Im}_n^2}$$

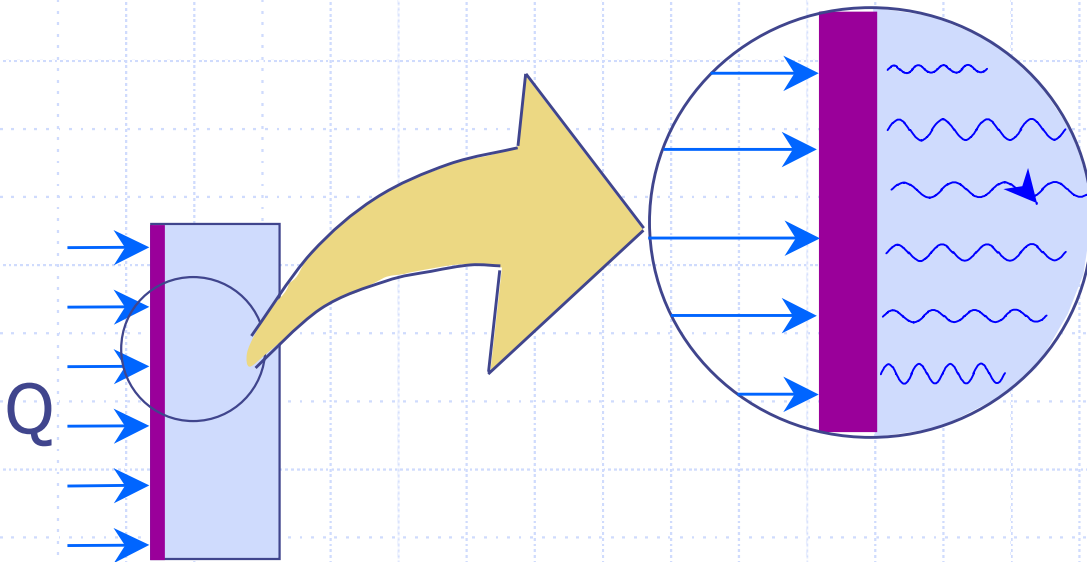


$$\phi = \tan^{-1} \left(\frac{\text{Im}_n}{\text{Re}_n} \right)$$



Synthetic Data

- ◆ Semi-infinite plate without defect



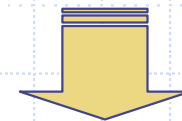
3D diffusion equation

$$\nabla^2 T - \frac{1}{\alpha} \frac{\partial T}{\partial t} = 0$$



1D solution

$$\frac{\partial^2 T}{\partial t^2} - \frac{1}{\alpha} \frac{\partial T}{\partial t} = 0$$

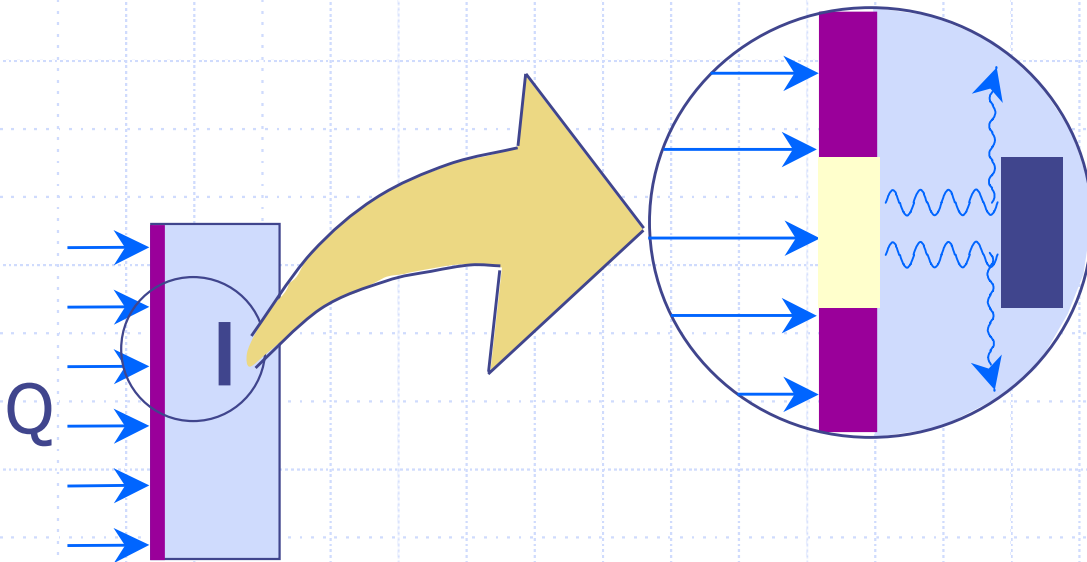


$$T = \frac{Q}{e\sqrt{\pi t}}$$



Synthetic Data

- ◆ Semi-infinite plate with defect



3D diffusion equation

$$\nabla^2 T - \frac{1}{\alpha} \frac{\partial T}{\partial t} = 0$$



2D solution

$$\nabla_{x,y}^2 T - \frac{1}{\alpha} \frac{\partial T}{\partial t} = 0$$

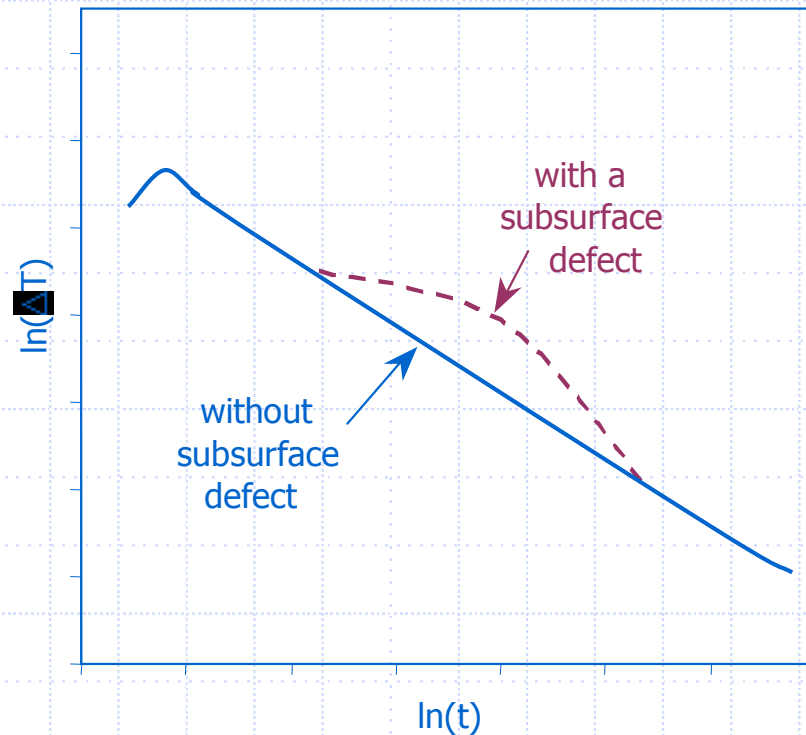


Synthetic Data

◆ Log-Log fitting

$$\mathcal{T} = \frac{Q}{e\sqrt{\pi t}}$$

$$\ln \mathcal{T} = \ln\left(\frac{Q}{e}\right) - \frac{1}{2} \ln(\pi t)$$





Synthetic Data

◆ Synthetic coefficients

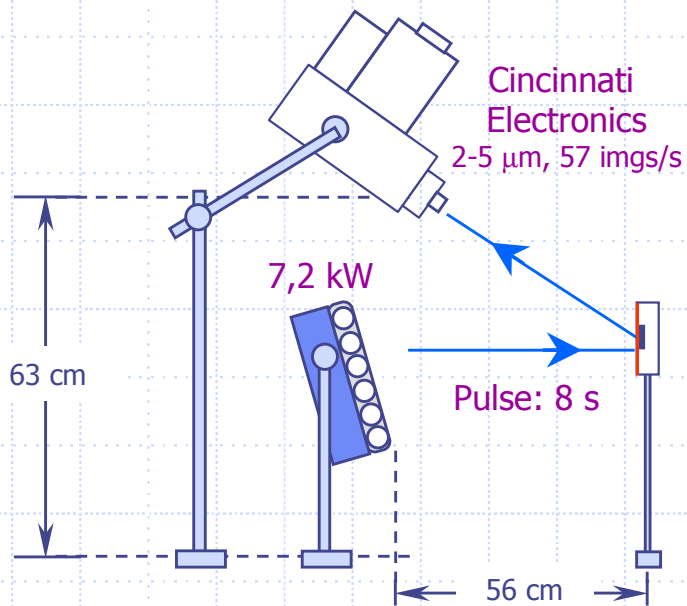
$$\ln T = a_0 + a_1 \ln(t) + a_2 \ln^2(t) + \dots + a_n \ln^n(t)$$

$$T(t) = \exp[a_0 + a_1 \ln(t) + a_2 \ln^2(t) + \dots + a_n \ln^n(t)]$$

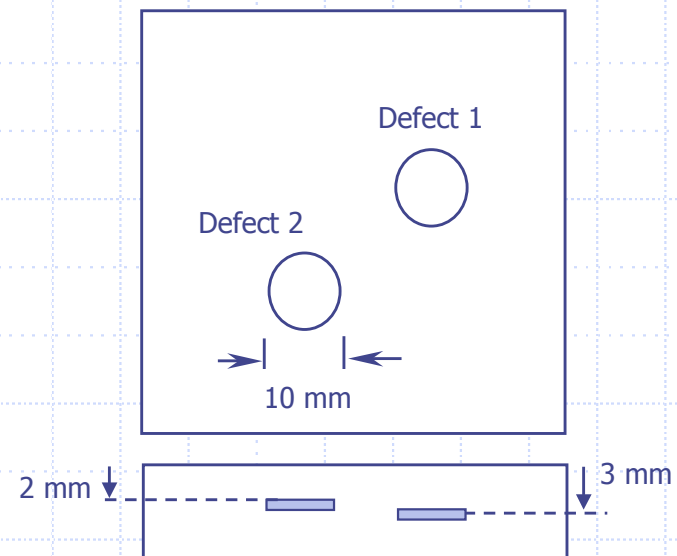


Experimental Results

◆ Case 1: Graphite-epoxy



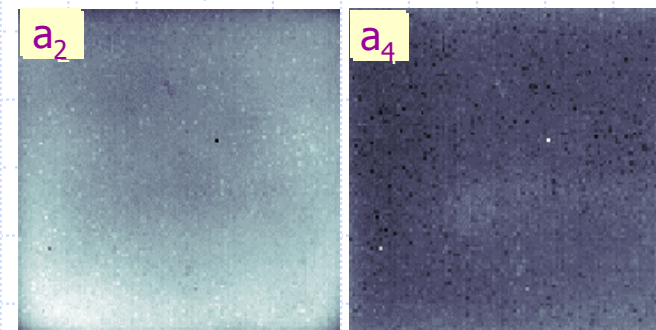
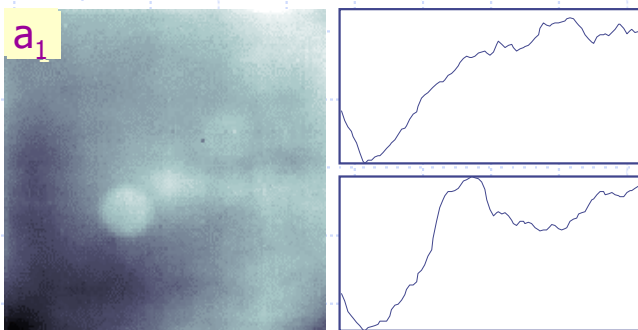
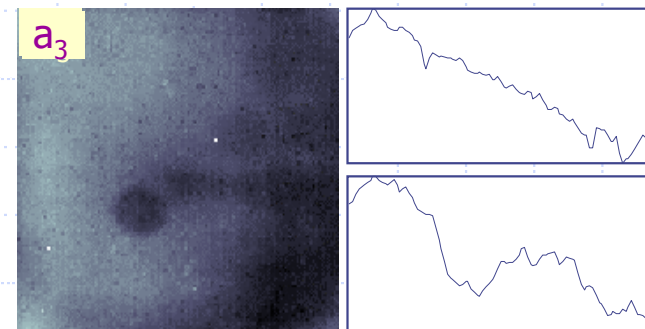
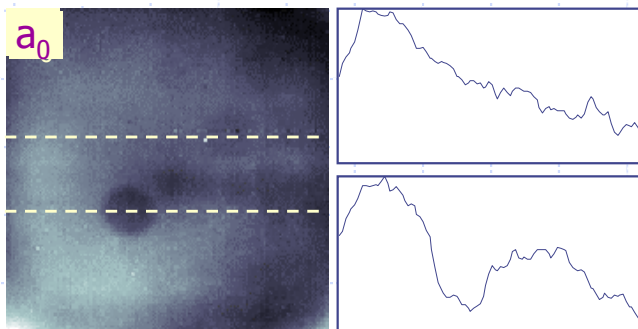
Graphite-epoxy
with 2 Teflon™ inclusions



Experimental Results

◆ Raw coefficients

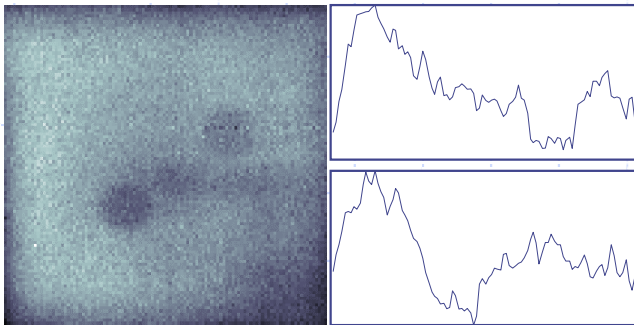
$$T(t) = \exp \left[a_0 + a_1 \ln(t) + a_2 \ln^2(t) + a_3 \ln^3(t) + a_4 \ln^4(t) \right]$$



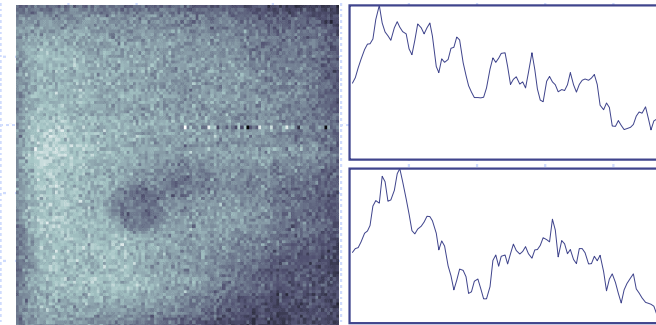
Experimental Results

◆ Direct PPT vs Synthetic PPT

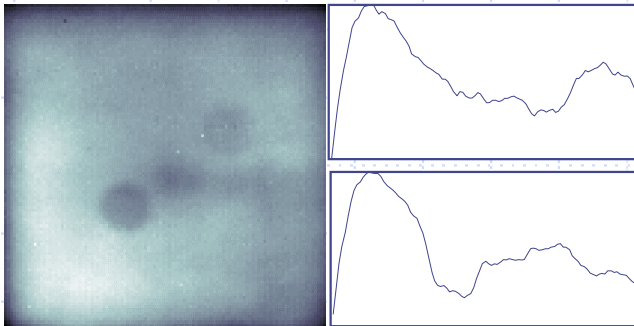
Direct PPT, $f=0.33$ Hz



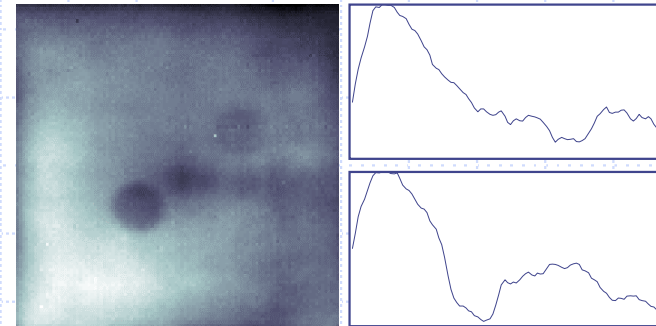
Direct PPT, $f=1.0$ Hz



Synthetic PPT, $f=0.33$ Hz

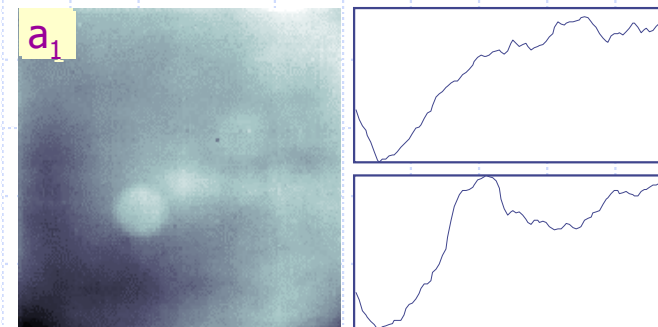
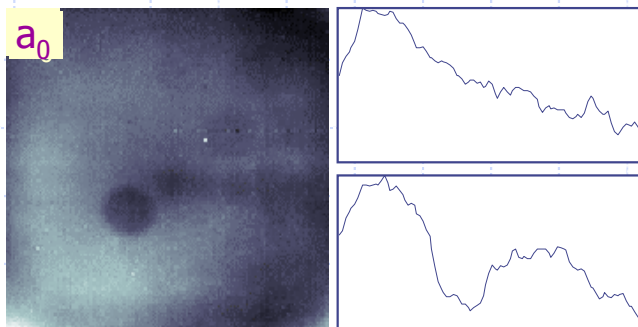


Synthetic PPT, $f=1.0$ Hz

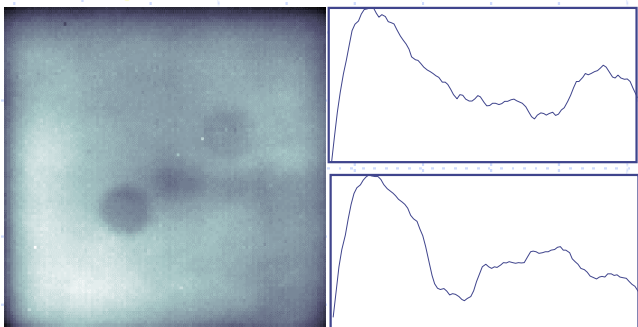


Experimental Results

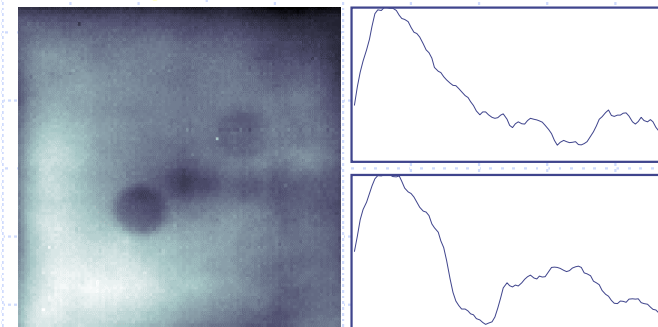
◆ Direct PPT vs Synthetic PPT



Synthetic PPT , $f=0.33$ Hz

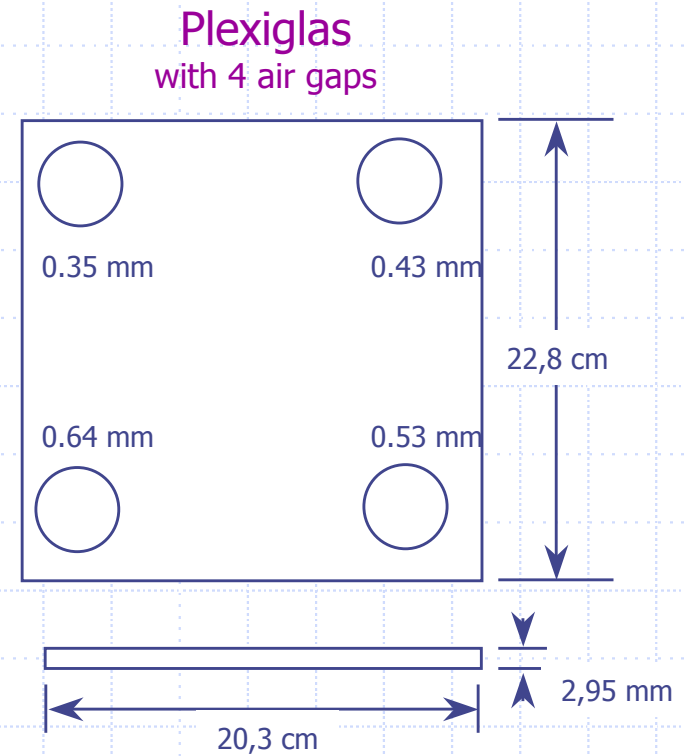
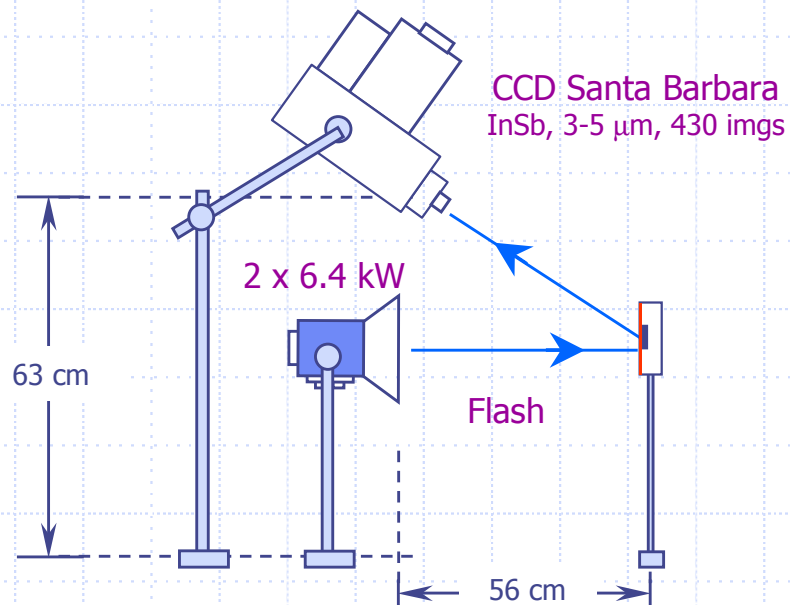


Synthetic PPT , $f=1.0$ Hz



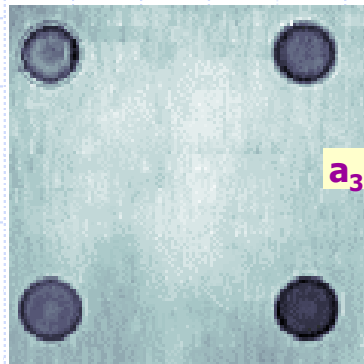
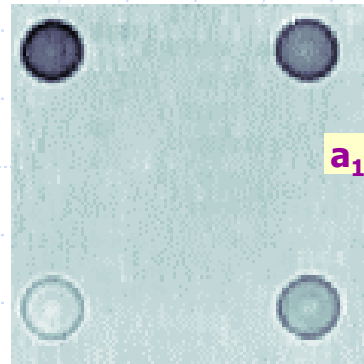
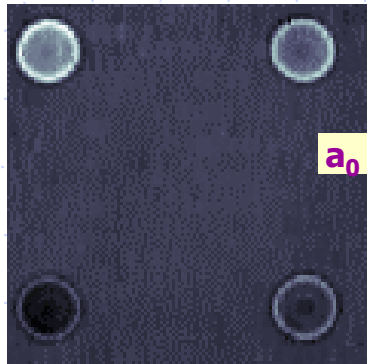
Experimental Results

◆ Case 2: Plexiglas



Experimental Results

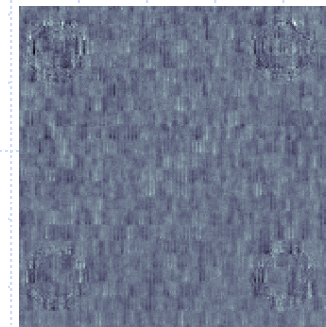
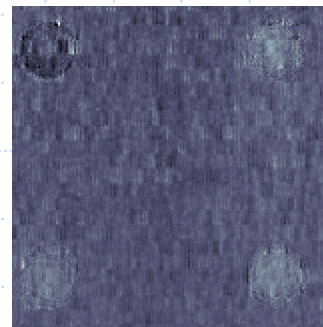
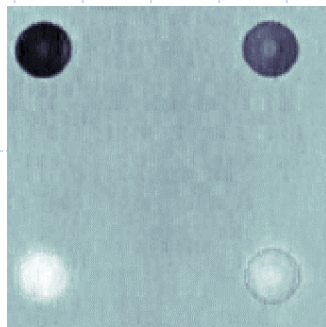
◆ Raw coefficients



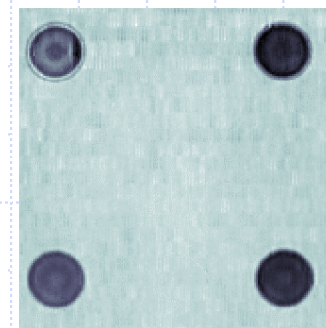
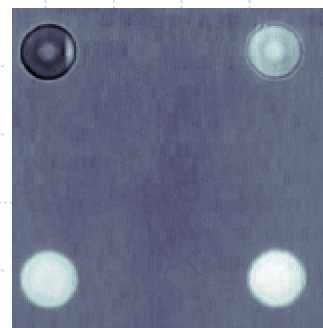
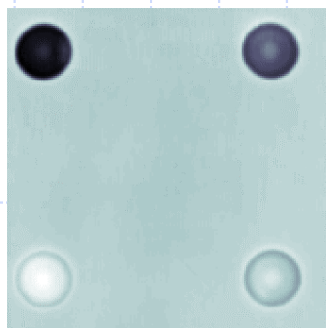
Experimental Results

◆ PPT vs synthetic

Direct PPT



Synthetic PPT



f=0.2 Hz

f=0.76 Hz

f=4.76 Hz



Conclusions & Perspectives

- ✓ Substantial data reduction;
- ✓ Possibility to work with analytical solutions;
- ✓ De-noising;
- ✓ Synthetic PPT images are OK for $f \uparrow$;
- ✗ Further processing of raw coefficients;
- ✗ Optimal polynomial degree;
- ✗ Depth measurement & defect characterization.

Thank you for your attention !

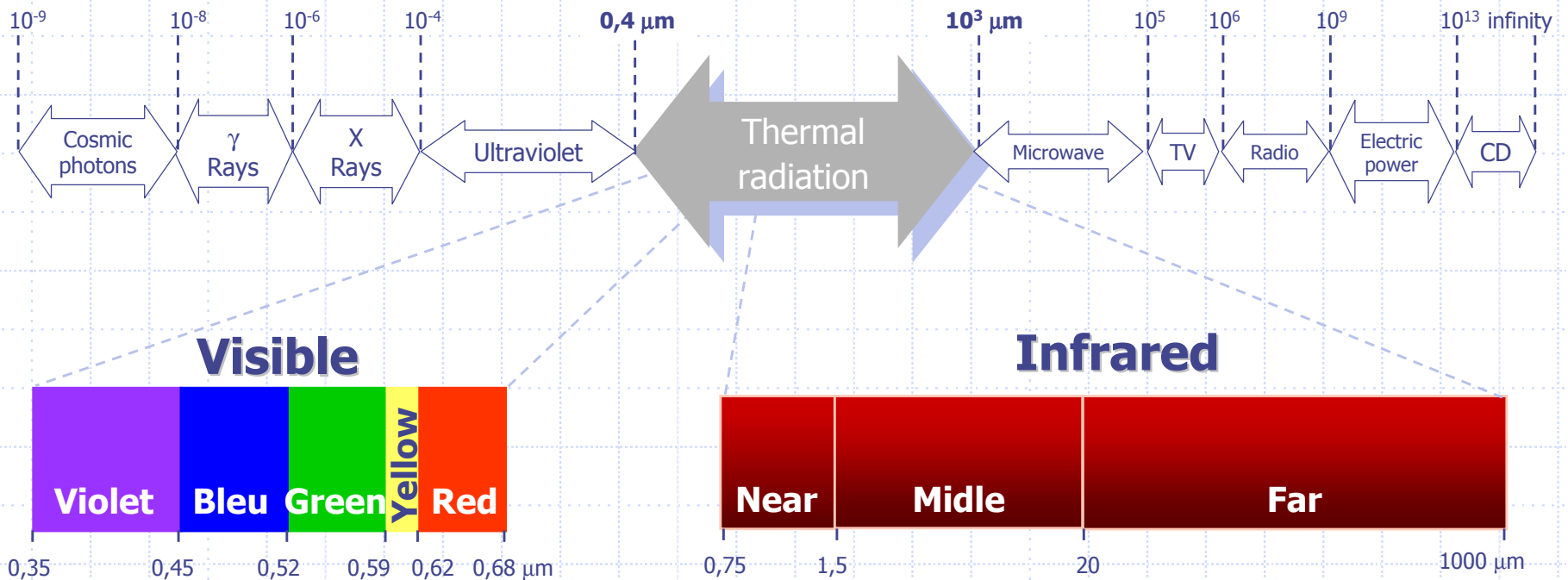
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Annexes

◆ Electromagnetic spectrum





Annexes

◆ Advantages & Limitations

- ✓ Fast surface inspection;
- ✓ Safety (no harmful radiations);
- ✓ Wide range of applications;
- ✓ Ease of deployment;
- ✓ No contact.
- × Non-uniform heating;
- × Specimen shape;
- × Thermal losses;
- × Cost of the equipment;
- × Limited thickness;
- × Emissivity problems.

Annexes

◆ Frequency response

